

Sheffield-Highgate Export Interface

SHEI



VSPC Quarterly Meeting
October 18, 2017

Northern Vermont Export Study Update

- VELCO is providing information to enable evaluation of potential solutions
 - Incremental export limit increases from system upgrades involving reactive support, transmission, subtransmission, and battery storage
 - Analyzed individual solutions and combinations of solutions
 - Can also provide initial construction cost estimates of transmission, synchronous condenser and battery options
- Distribution utilities (DUs) purview
 - Estimate other options
 - Evaluate options with respect to their potential for increasing energy sales
 - Lead selection process for preferred options



Chronology

- July 12, 2017 — SHEI study kickoff and information sharing
<https://www.vermontspc.com/grid-planning/shei-info>
https://www.vermontspc.com/library/document/download/5810/20170712_SHEI_Preso_MtgVersion.pdf
- September 1, 2017 — study update
<https://www.vermontspc.com/library/document/download/5894/SHEI%20Study%20SeptemberUpdate.pdf>
- September 11, 2017 — study update makeup session
<https://www.vermontspc.com/library/document/download/5894/SHEI%20Study%20SeptemberUpdate.pdf>

System conditions tested

- Vermont load at 700 MW (about 55 MW inside SHEI)
- Summer long term emergency (LTE) ratings
- SHEI Wind plants at full output (105 MW)
- Newport block load served from Canada
- Highgate converter at 227 MW across the US/Canada border
- All-lines-in condition (N-1 testing)
- Five representative outages (N-1-1 testing)
 - Essex STATCOM
 - Sand Bar-Georgia K19 115 kV line
 - St Johnsbury-Lyndonville K28 115 kV line
 - Stowe 115/34.5 kV transformer
 - Marshfield-Plainfield 3317 34.5 kV line

Power flow study approach (two types of export limits)

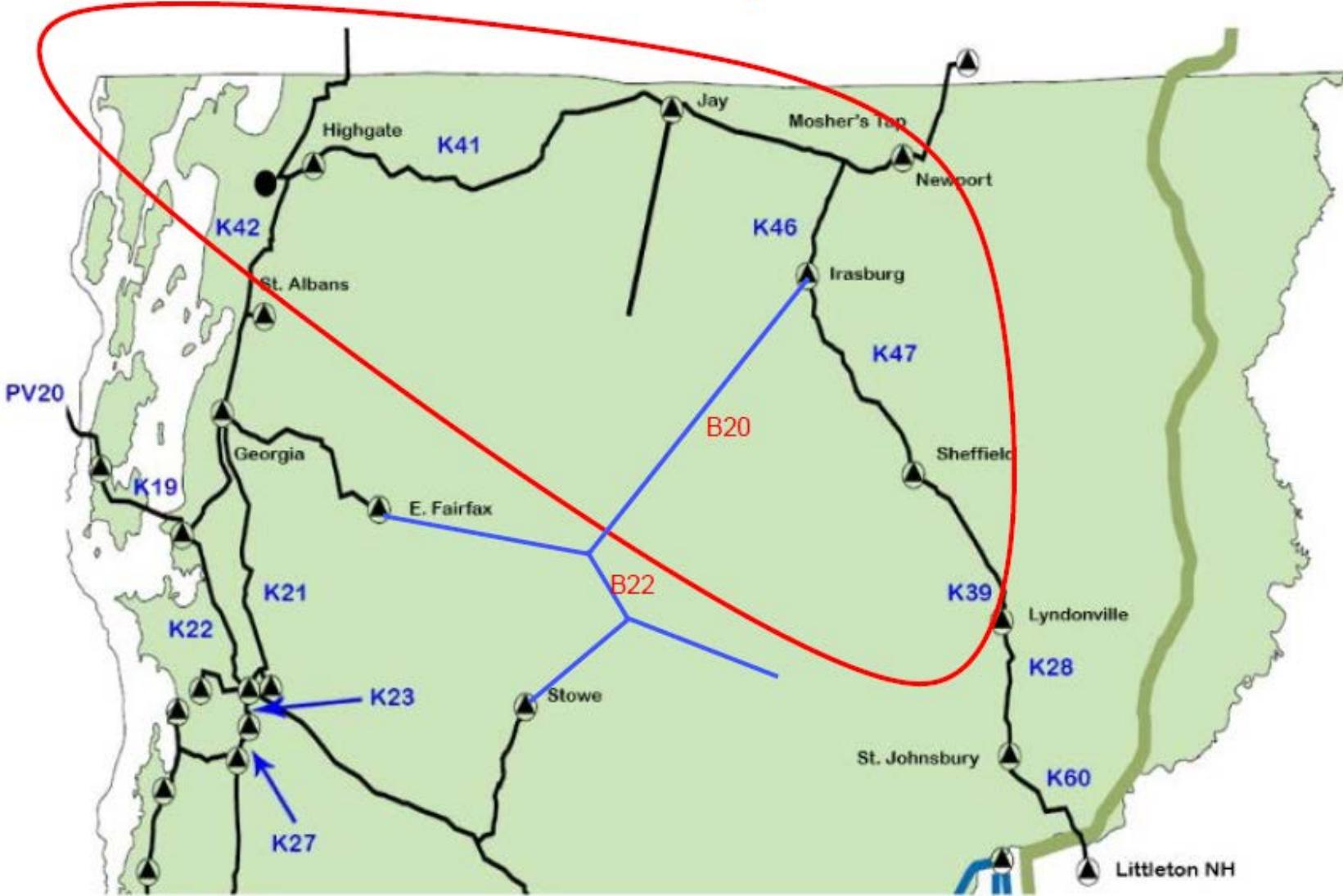
- Determine voltage export limit (at 95% of nominal voltage, or voltage collapse)
 - Adjust generation and Highgate imports until voltage limit is reached
 - Trip 34.5 kV lines when they are overloaded
 - Avoid tripping 34.5 kV lines when such tripping would cause a voltage collapse
 - Voltages can be above acceptable levels in these cases
 - Reduce SHEI load if voltage limit is not reached with maximum generation
 - This happens for the most robust options
- Determine thermal export limit for all-lines-in case and Essex STATCOM-out case based on 100% summer emergency ratings
 - Ignore 115 kV line overloads south of Georgia and Sand Bar
 - Assuming that they can be addressed by reducing PV20 flows from New York

Notes

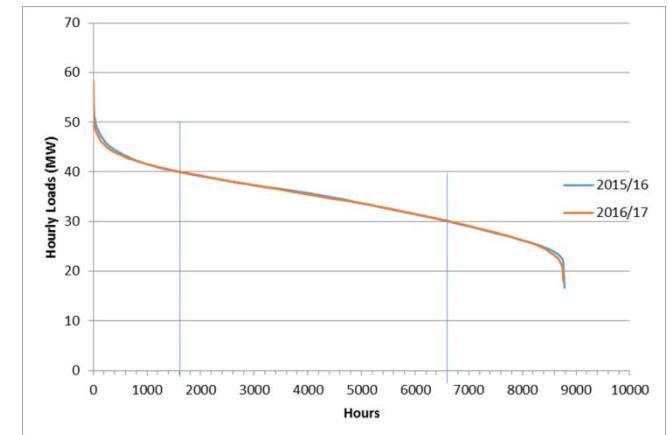
- MW export limit results should only be used to calculate incremental benefit (within +/- 5 MW) of each case/scenario
 - ISO-NE is responsible for determining system limits
 - ISO-NE cases may model different system assumptions
 - Essex STATCOM, capacitor bank dispatch, load distribution, tie flows
 - Case 0 results are the benchmarks within each column of results
- Utilized the same ISO-NE interface definition
 - Did not postulate how system operation (SHEI definition) or market implications would change following an upgrade
- Voltage limits are based on voltage collapse or low voltage at Highgate or St Albans 115 kV
- Thermal limits are based on overloads on K42, B20 or B22
 - B20 overloads when not upgraded
 - B22 overloads when the B20 line is upgraded

The Sheffield-Highgate Export Interface (SHEI)

ISO-NE determines the SHEI limits at or below which the system can withstand an anticipated system outage



- Average load is 35 MW
 - Between 20 MW and 60 MW
- Analysis of total generation production data is less useful
 - Affected by system limits, operating actions, internal plant constraints, and markets
- ISO curtailments more likely during spring and during transmission outages
 - Also less likely during summer



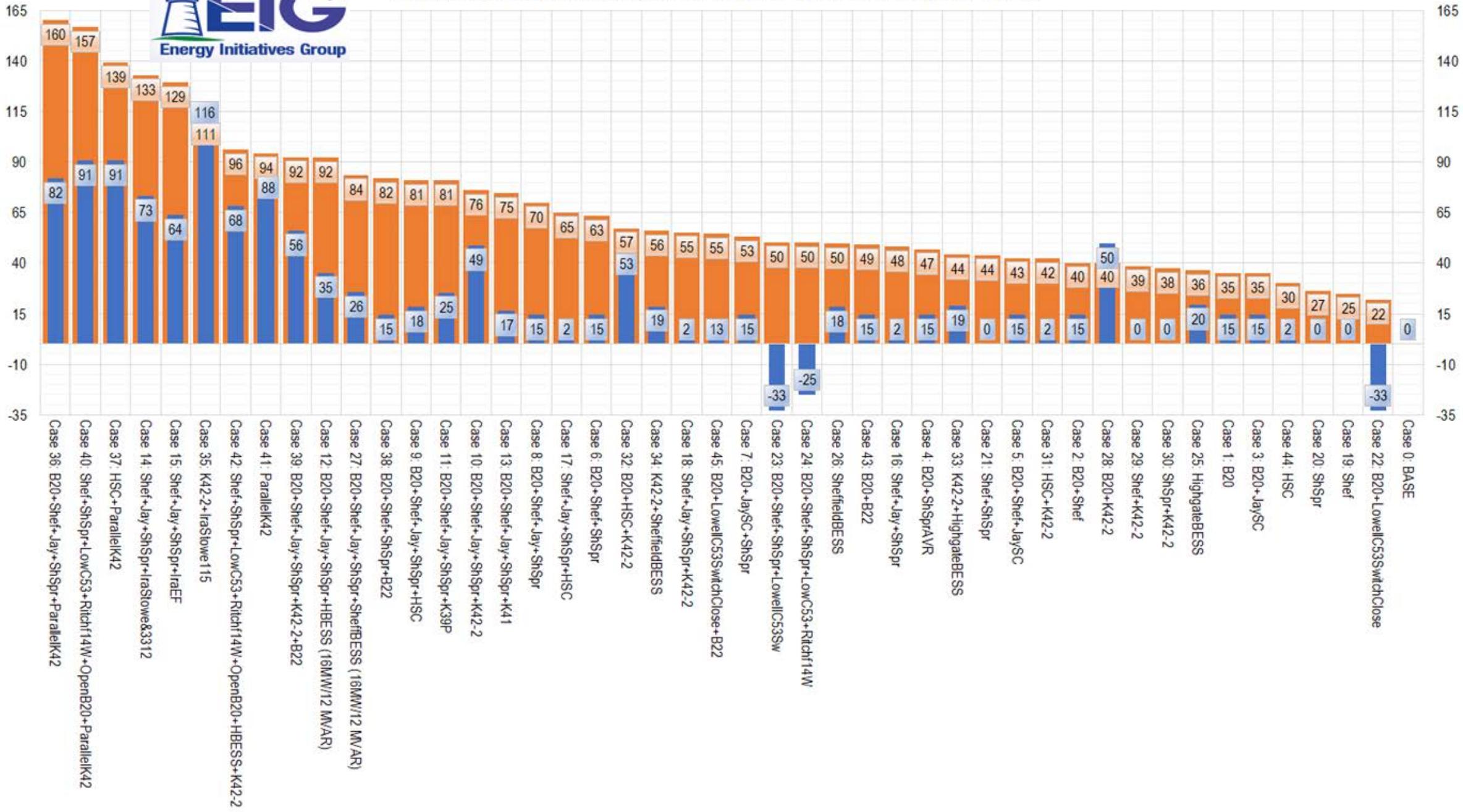
Initial study scope

Options	Description	Cases																	
		0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
1	Reconducto the B20 34.5 kV line and upgrade the Lowell 46/34.5 kV transformer	X	X	X	X	X	X	X	X	X	X	X	X	X	X				
2	Enable voltage control at Sheffield		X			X	X			X	X	X	X	X	X	X	X	X	X
3	Recognize the Jay synchronous condenser 1.15 service factor			X		X		X		X	X	X	X	X	X	X	X	X	X
4	Enable voltage control at Sheldon Springs				X			X	X	X	X	X	X	X	X	X	X	X	X
5	Install a 15 MVAr synchronous condenser at Highgate 115 kV										X								X
6	Reconducto K42 Highgate-St Albans 115 kV line												X						X
7	Install a 2nd 115 kV line alongside K39													X					
8	Install a 16 MW/12 MVAr battery energy storage system (BESS) at Highgate 115 kV														X				
9	Reconducto K41 Highgate-Jay 115 kV line															X			
10	Install a new Irasburg to Stowe 115 kV line																X		
11	Install a new Irasburg to East Fairfax 115 kV line																	X	

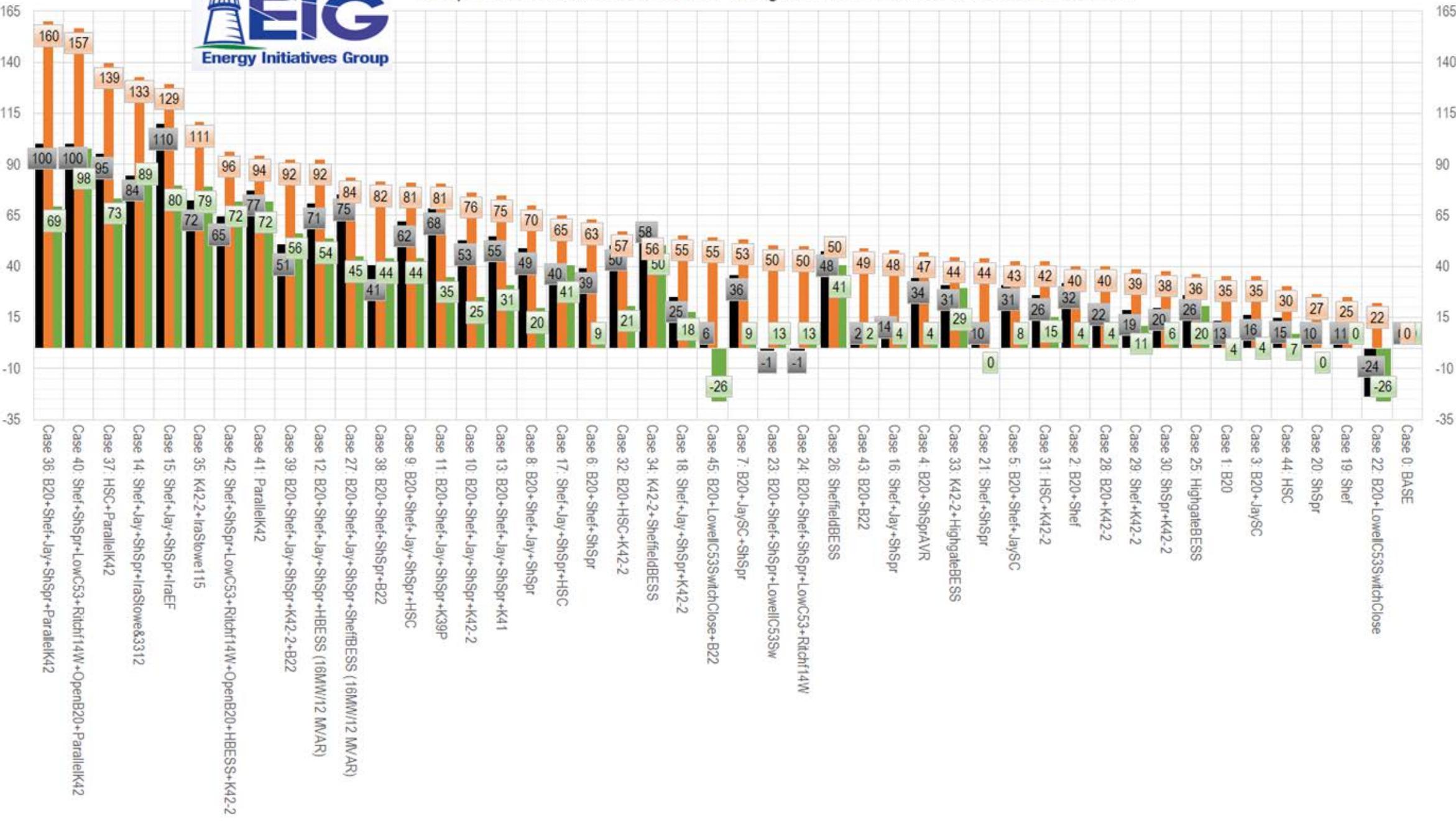
Additional cases tested

Opt #	Upgrade elements	Cases																											
		19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	
1	B20 upgrade (line and Lowell transformer)			X	X	X			X	X			X				X		X	X				X		X			
2	Enable the Sheffield AVR	X	X	X	X				X	X								X		X	X	X		X					
3	Recognize Jay synch cond 1.15 service factor								X										X			X							
4	Enable the Sheldon Springs AVR	X	X		X	X			X		X							X		X	X	X	X		X				
5	Install a 15MVA synch cond at Hgate 115 kV											X	X		X	X				X							X		
6	Reconductor K42 Hgate-St Albans 115 kV line										X	X	X	X	X	X	X					X			X				
7	Install a 2nd K39 Sheffld-Lyndonvil 115 kV line																												
8	15 MVA Storage at Highgate 115 kV									X								X									X		
9	Reconductor K41 Highgate-Jay 115 kV line																												
10	Install a new Irasburg to Stowe 115 kV line																			X									
11	Install a new Irasburg to E Fairfax 115 kV line																												
12	Close the normally open Lowell C53 switch		X	X	X																			X	X		X		
13	Close Ritchford 14W & upgrade RF-HG46kV					X																		X	X				
14	15 MVA battery storage at Sheffield 115 kV								X	X								X											
15	Install a 2nd 115 kV line alongside line K42																				X	X		X	X				
16	Upgrade 1.7 miles of B22 line to 39 MVA																				X	X			X	X		X	X
17	Open B20 line at Johnson																						X	X			X	X	

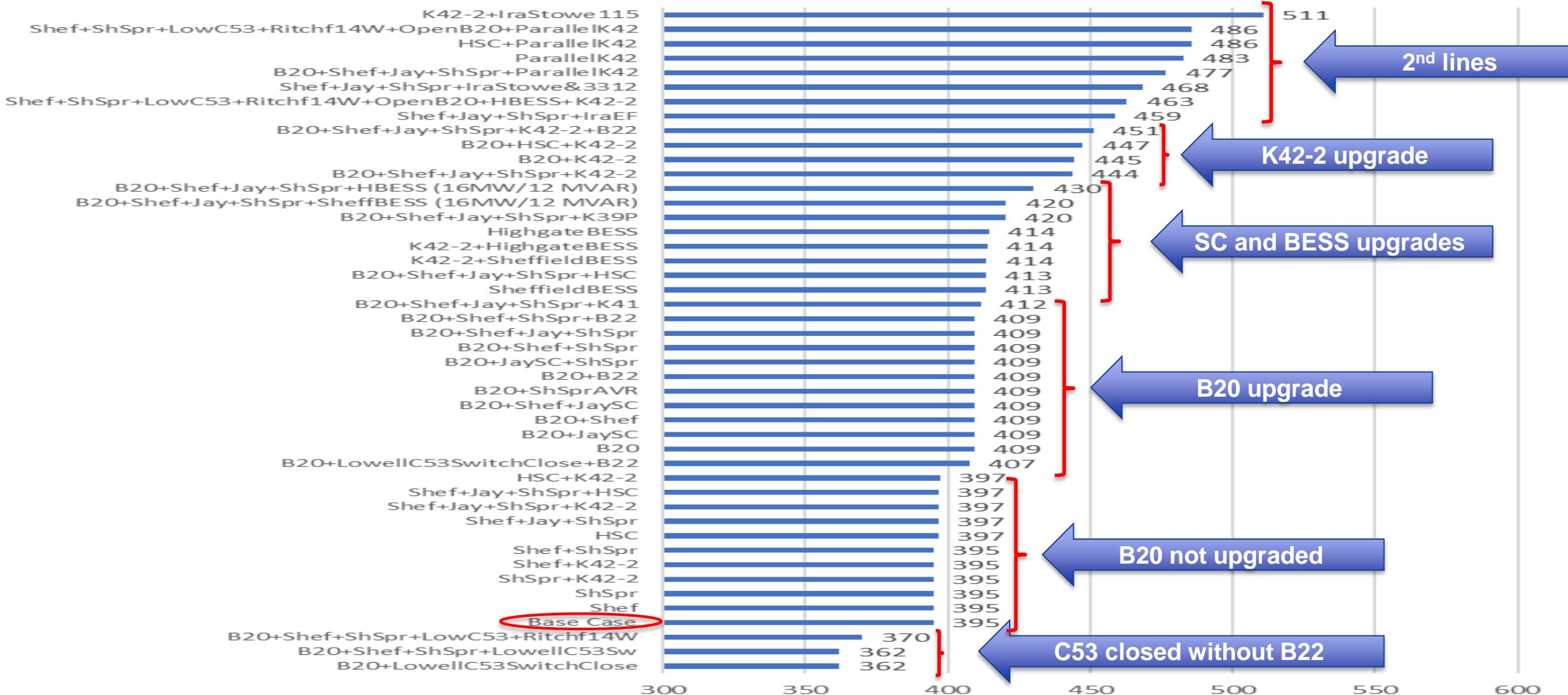
Comparison of Delta (Incremental) SHEI From Base - All Lines In: Voltage vs. Thermal



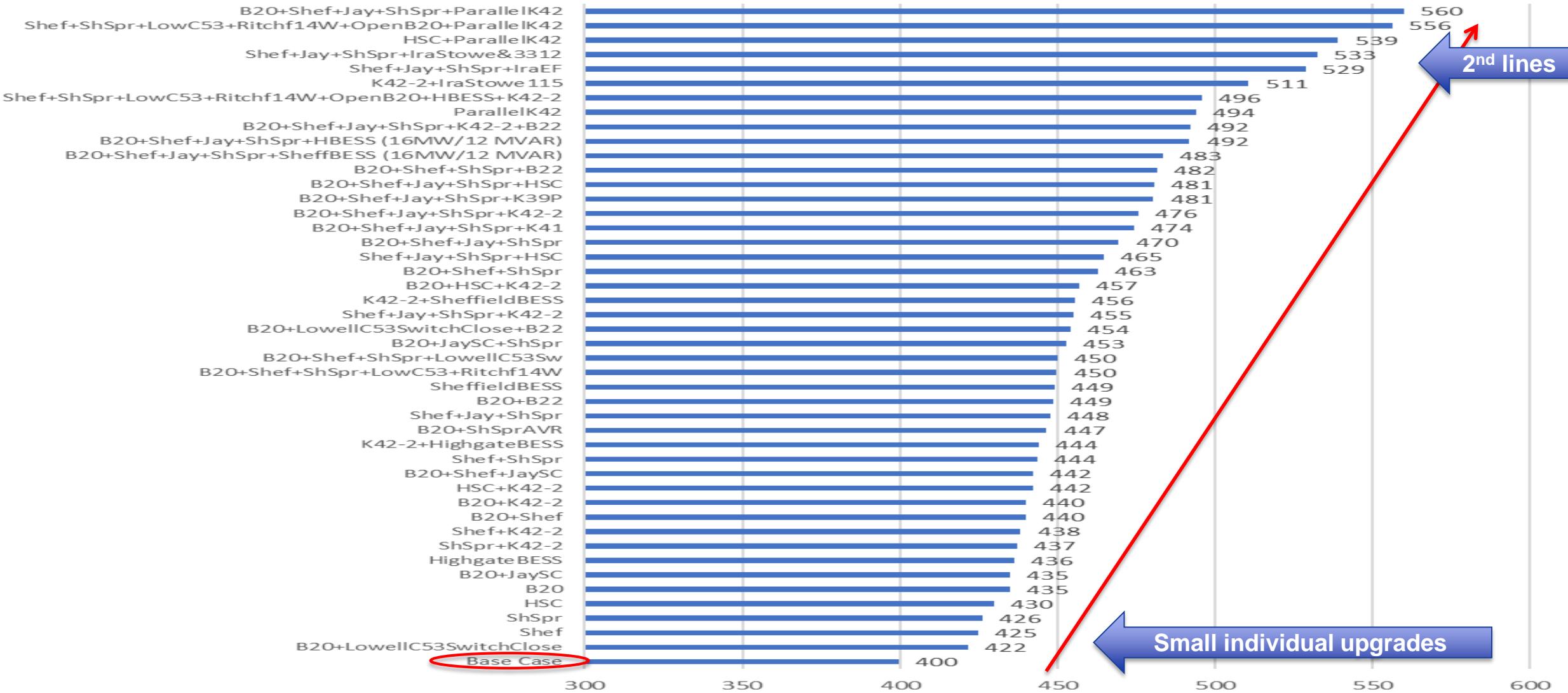
Comparison of Delta SHEI From Base - Voltage: ALI vs. Essex STATCOM OOS vs. K19 OOS



Study Results – Thermal SHEI_TH in MW



Study Results – Voltage SHEI_V in MW



Highlights

- Multiple options can increase voltage limit
 - Utilizing capability of existing resources (Sheldon Springs AVR, Sheffield AVR) worth pursuing
- Highgate synchronous condenser (SC) provides 30 MW of incremental voltage benefit, but minimal thermal benefit
 - Combining Highgate SC with thermal upgrades can achieve reasonably high thermal and voltage improvements
 - Highgate battery performs better than SC because it acts like an SC with MW load increase
- Options that add a new 115 kV line are longer term options

More highlights

- B20 upgrade provides 35 MW of incremental voltage benefit and 15 MW of thermal benefit
 - B22 line will be limiting if B20 line is upgraded — B22 upgrade provides an additional 14 MW of voltage benefit, but no thermal benefit
 - Closing Lowell C53 switch has a negative impact if B22 line is not upgraded
 - in general, forcing more power through subtransmission system can be a concern in terms of overall system performance
- Thermal benefit of B20 and B22 is limited by K42-2 line section
 - Upgrading K42-2 with B20 and B22 raises thermal limit by over 50 MW
- K42-2 upgrade provides minimal voltage benefit unless redesigned to achieve lower reactance

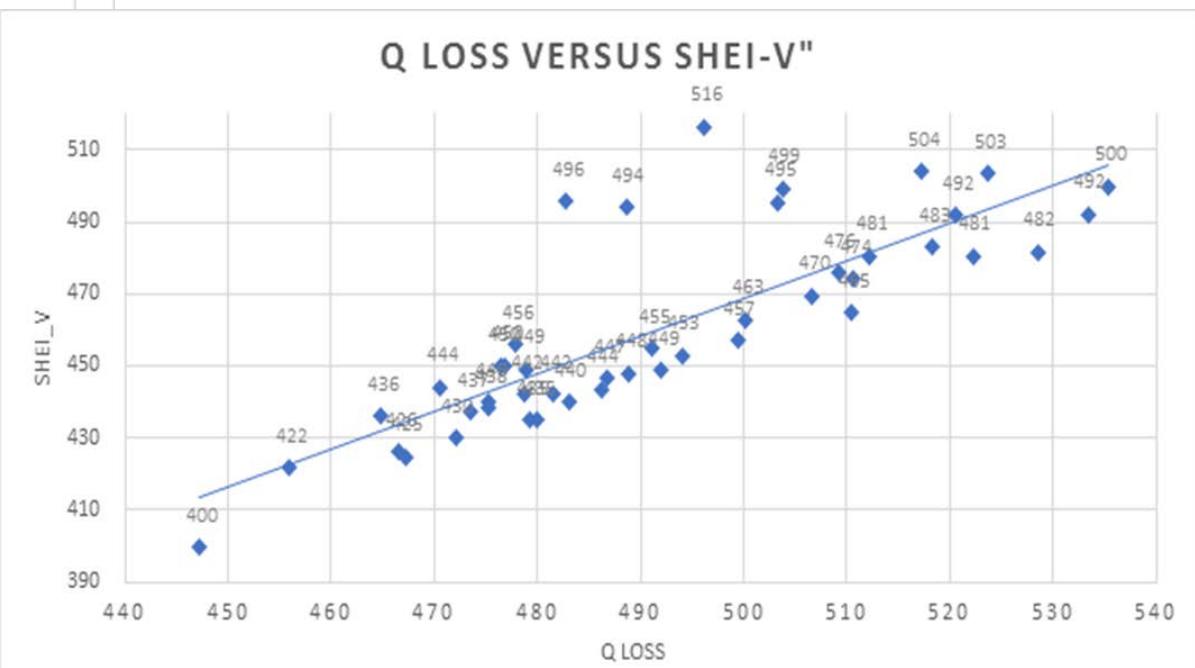
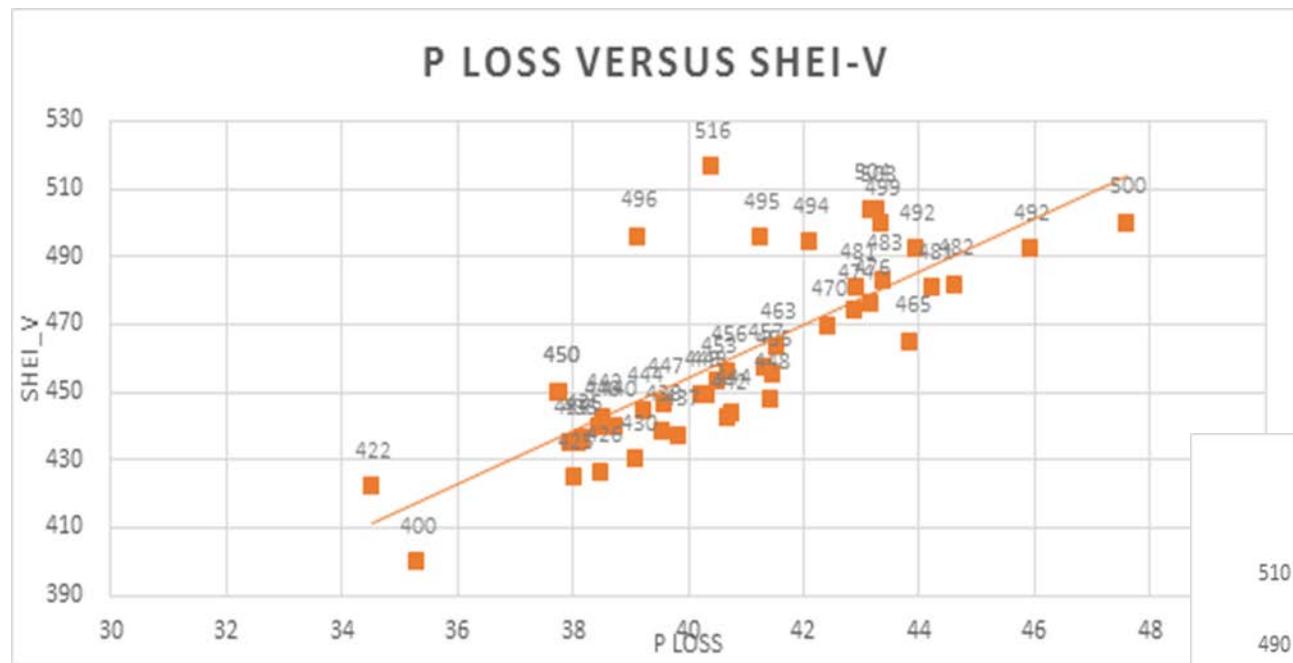
VELCO K42 asset condition evaluation

- K42 line was assessed in September
 - 16.75 miles from Highgate to Georgia, and 9.9 miles for limiting section
 - 50% of poles need to be replaced
 - Almost all poles will need to be replaced between 3 years and 15 years from now
- VELCO will determine whether it makes sense to rebuild entire line sooner rather than rebuilding it piecemeal
 - Construction efficiency leading to reduced cost for overall project
 - Line cannot be out of service for long periods of time
 - Opportunity to reduce losses (K42 is the most lossy line in Vermont)
 - Opportunity to further address SHEI concerns and facilitate reaching VT's long term renewable energy goals

What next after this technical analysis?

- Possible approaches to estimate benefit of options or combination of options that were not tested
 - Calculate incremental benefits of individual options as they are added to various combinations, and average these delta benefits
 - Perform regression analyses
 - To extract expected benefit of each option or combination of options
 - To highlight which options may be more significant than others
 - To construct a predictive model for estimating MW value of untested option combinations
- Considerations beyond incremental MW export
 - Other system benefits, real and reactive losses, robustness, operational flexibility, feasibility, asset condition, timing, aesthetic and environmental impacts, cost, market considerations, etc.

Loss comparison of cases



Regression Results SHEI_V

- Format of regression

$$Y = b + a_1 * X_1 + a_2 * X_2 + a_3 * X_3 + \dots$$

- Dependent variable "Y" represents SHEI_V
- Independent variables "X" are modeled as a logical (1 or 0) for each upgrade option
- Coefficients (a_1, a_2, a_3 , etc.) are in MW

- P-value is a measure of significance

- Less than 0.05 is significant (highlighted green)
- Greater than 0.05 is not significant (highlighted yellow or red)

- Intercept ("b") is 409.8 MW

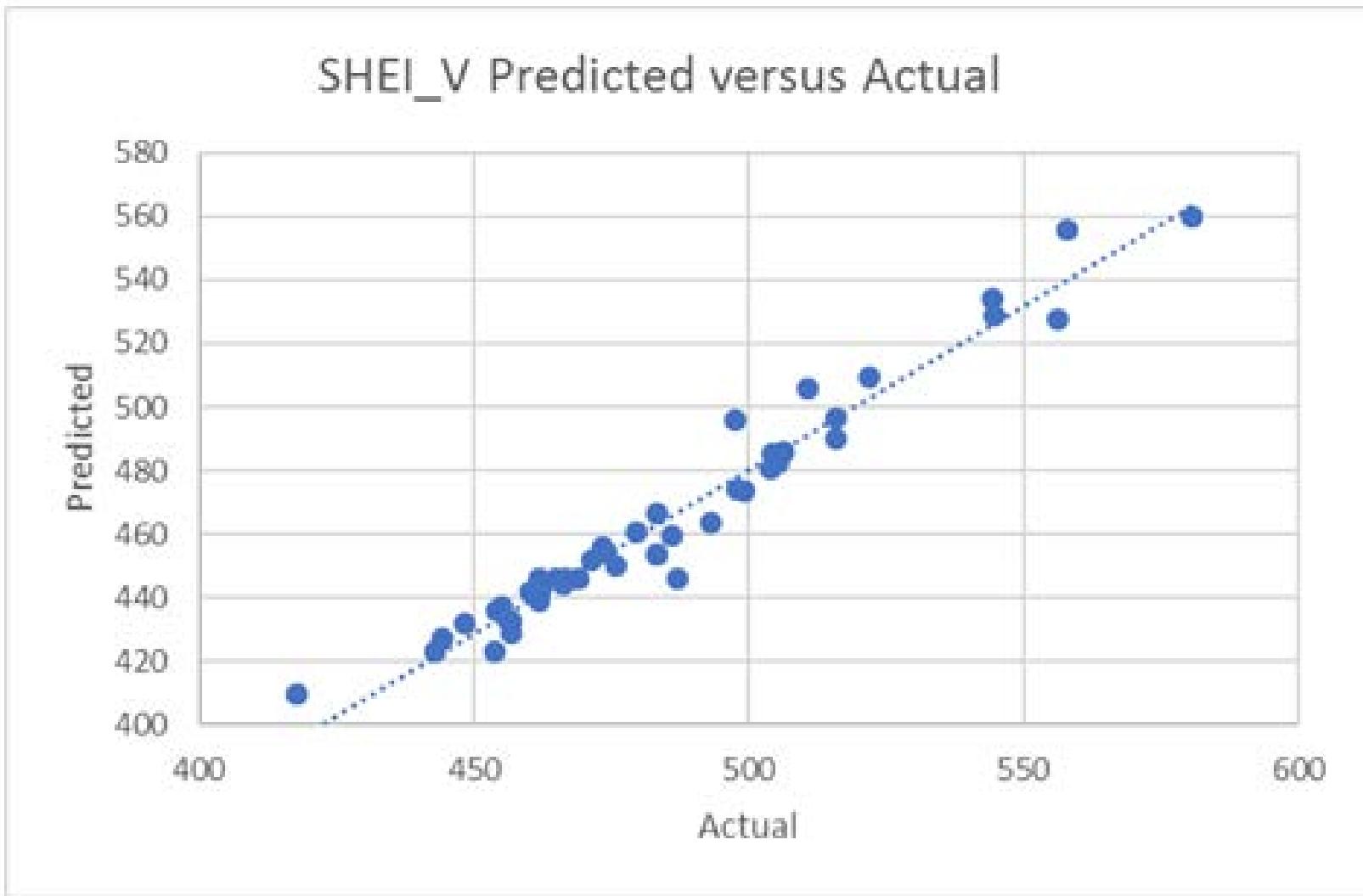
- From the table we can calculate the predicted effect of building a line parallel to K42 from Highgate to St Albans tap (Coefficient is 96.1 MW)

$$\text{SHEI}_V = 409.8 + (96.1 * 1) = 505.9 \text{ MW}$$

- For Case 41, actual load flow results calculated 494 MW (2.4% less)

	<i>Coefficients</i>	<i>P-value</i>
Intercept	409.801	0.000
B20	19.041	0.000
Sheffield	13.513	0.000
Jay SC	3.952	0.098
Sheldon	17.220	0.000
Highgate SC	21.853	0.000
K42-2	10.009	0.000
2 nd K39	16.973	0.003
Highgate	26.218	0.000
K41	10.673	0.055
Irasburg-	89.503	0.000
Irasburg-	84.415	0.000
Lowell C53	(5.996)	0.061
Sheffield	22.646	0.000
Parallel K42	96.109	0.000
B22	22.950	0.000
Open B20	25.345	0.000

Regression Results Predicted Versus Actual



Characteristics of selected solution

- Coincident with timing and duration of curtailments
 - Every season, mostly spring and except perhaps in summer
 - Any time of day
- Able to respond to variability of wind power
- Dependable
- Implemented in a timely fashion
- Cost effective (expenditures lower than projected revenue gains)
 - Ranking based on payback, \$/MW, cost-benefit, ...
 - Analysis can include system loss benefits, asset condition improvements, other system benefits, and qualitative assessments

Proposed next steps

- VELCO participation
 - Transmission option cost estimates (lines, battery, SC)
 - Further assistance as requested by DUs
 - Evaluate T&D study cost options
- DUs conduct further analysis and develop process for solution selection
 - Estimate cost of subtransmission upgrades and other options
 - Non-wires alternatives
 - Economic evaluation of solutions
 - Solution selection
 - Regulatory process (with VELCO testimony on transmission system impacts as needed)
- Recommend estimating all options using common assumptions
 - VELCO tools are available

Results tables

APPENDIX

Thermal MW export limit results (based on overloads)

	Benchmark case 0 – No upgrades -->	All lines in	Essex STATCOM out
		395 MW	379 MW
<u>CASES</u>	<u>Upgrades</u>	Incremental over benchmark	
1	B20	15 MW	14 MW
2	B20+Sheffield AVR	15	23
3	B20+Jay Synchronous Condenser	15	16
4	B20+Sheldon Springs AVR	15	26
5	B20+Sheffield AVR+Jay Synchronous Condenser	15	23
6	B20+Sheffield AVR+Sheldon Springs AVR	15	26
7	B20+Jay Synchronous Condenser+Sheldon Springs AVR	15	26
8	B20+Sheffield AVR+Jay SC+Sheldon Springs AVR	15	28
9	B20+Sheffield+Jay SC+Sheldon Springs+Highgate Sync Cond	18	31
10	B20+Sheffield AVR+Jay SC+Sheldon Springs AVR+K42-2	49	51
11	B20+Sheffield AVR+Jay SC +Sheldon Springs AVR+ 2 nd K39	25	37
12	B20+Shef+Jay+ShSpr+HighgateBattery (16MW/12 MVAR)	35	45
13	B20+Sheffield AVR+Jay SC+Sheldon Springs AVR+K41	17	28
14	Shef+Jay+Sheldon Springs+ New Irasburg Stowe&3312	73	89
15	Shef+Jay+Sheldon Springs+ New Irasburg E Fairfax	64	75
16	Sheffield AVR+Jay SC+Sheldon Springs AVR	2	15
17	Sheffld+Jay SC+Sheldon Springs+Highgate Sync Condenser	2	15
18	Sheffield AVR+Jay SC+Sheldon Springs AVR+K42-2	2	15

Voltage MW export limit results (based on low voltage)

		All lines in	Essex STAT out	K19 out	K28 out	Stowe transfrm out	3317 (MP) out
	Benchmark case 0 – No upgrades →	400 MW	379 MW	367 MW	253 MW	399 MW	410 MW
CASES	Upgrades	Incremental over benchmark					
1	B20	35 MW	13 MW	4 MW	7 MW	41 MW	40 MW
2	B20+Sheffield AVR	40	32	4	33	49	48
3	B20+JaySC	35	16	4	22	41	43
4	B20+Sheldon Springs AVR	47	34	4	29	49	46
5	B20+Sheffield+JaySC	43	31	8	33	49	48
6	B20+Sheffield+Sheldon Springs	63	39	9	33	51	48
7	B20+JaySC+Sheldon Springs	53	36	9	29	47	48
8	B20+Sheffield+Jay+Sheldon Springs	70	49	20	33	53	50
9	B20+Sheffield+Jay+Sheldon Springs+Highgate SC	81	62	44	33	73	70
10	B20+Sheffield+Jay+Sheldon Springs+K42-2	76	53	25	33	65	64
11	B20+Sheffield+Jay+Sheldon Springs+K39P	81	68	35	33	68	64
12	B20+Shef+Jay+ShSpr+HgateBESS (16MW/12 MVAR)	92	71	54	63	77	75
13	B20+Sheffield+Jay+Sheldon Springs+K41	75	55	31	33	58	62
14	Shef+Jay+Sheldon Springs+Irasburg Stowe&3312	133	84	89	206	102	94
15	Shef+Jay+Sheldon Springs+Irasburg E Fairfax	129	110	80	206	100	90
16	Sheffield+Jay+Sheldon Springs	48	14	4	23	39	32
17	Sheffield+Jay+Sheldon Springs+Highgate SC	65	40	41	23	57	56
18	Sheffield+Jay+Sheldon Springs+K42-2	55	25	18	23	49	44

MW export limit results for the additional cases

CASES	Upgrades	Benchmark case 0 – No upgrades -->	All lines in Thermal	All lines in Voltage	Essex STATCOM out Voltage	K19 out Voltage
			400 MW	395 MW	379 MW	367 MW
19	Sheffield AVR		0 MW	25 MW	11 MW	0 MW
20	Sheldon Springs AVR		0	27	10	0
21	Sheffield AVR + Sheldon Springs AVR		0	44	10	0
22	B20+LowellC53SwitchClose		-33	22	-24	-26
23	B20+Sheffield+Sheldon Springs+LowellC53Switch		-33	50	-1	13
24	B20+Sheffield+Shelson Springs+LowellC53+Ritchford14W		-25	50	-1	13
25	Highgate BESS (16MW/12 MVAR)		20	36	26	20
26	Sheffield BESS (16MW/12 MVAR)		18	50	48	41
27	B20+Shef+Jay+ShSpr+Sheffield BESS (16MW/12 MVAR)		26	84	75	45
28	B20+K42-2		50	40	22	4
29	Sheffield AVR+K42-2		0	39	19	11
30	Sheldon Springs AVR+K42-2		0	38	20	6
31	Highgate Synchronous Condenser+K42-2		2	42	26	15
32	B20+Highgate Synchronous Condenser+K42-2		53	57	50	21
33	K42-2+Highgate BESS (16MW/12 MVAR)		19	44	31	29
34	K42-2+Sheffield BESS (16MW/12 MVAR)		19	56	58	50
35	K42-2+Irasburg to Stowe 115 line		116	111	72	79

MW export limit results for the additional cases

	Benchmark case 0 – No upgrades -->	All lines in Thermal	All lines in Voltage	Essex STATCOM out Voltage	K19 out Voltage
		400 MW	395 MW	379 MW	367 MW
CASES	Upgrades	Incremental over benchmark			
36	B20+Sheffield AVR+Jay SC+Sheldon Spr AVR+ParallelK42	82 MW	160 MW	100 MW	69 MW
37	Highgate Synchronous Condenser+Parallel K42 line	91	139	95	73
38	B20+Sheffield AVR+Sheldon Springs AVR+B22	15	82	41	44
39	B20+Sheffield AVR+Jay SC+Sheldon Spr AVR+K42-2+B22	56	92	51	56
40	Shef+ShSpr+LowC53+Ritchf14W+OpenB20+ParallelK42 line	91	157	100	98
41	Parallel K42 line	88	94	77	72
42	Shef+ShSpr+LowC53+Ritchf14W+OpenB20+HBESS+K42-2	68	96	65	72
43	B20+B22	15	49	2	2
44	Highgate Synchronous Condenser	2	30	15	7
45	B20+LowellC53SwitchClose+B22	13	55	6	-26